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**Squire et al.**

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[54] **STENT SLIP SENSING SYSTEM AND METHOD**

[75] Inventors: **James C. Squire, Everett; Campbell Rogers, Westwood; Elazer R. Edelman, Brookline, all of Mass.**

[73] Assignee: **Massachusetts Institute of Technology, Cambridge, Mass.**

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- [51] **Int. Cl.<sup>7</sup>** ..... **A61F 11/00**
- [52] **U.S. Cl.** ..... **600/381; 600/373; 606/108**
- [58] **Field of Search** ..... **600/373, 381; 606/108, 192, 194, 195, 198; 128/899**

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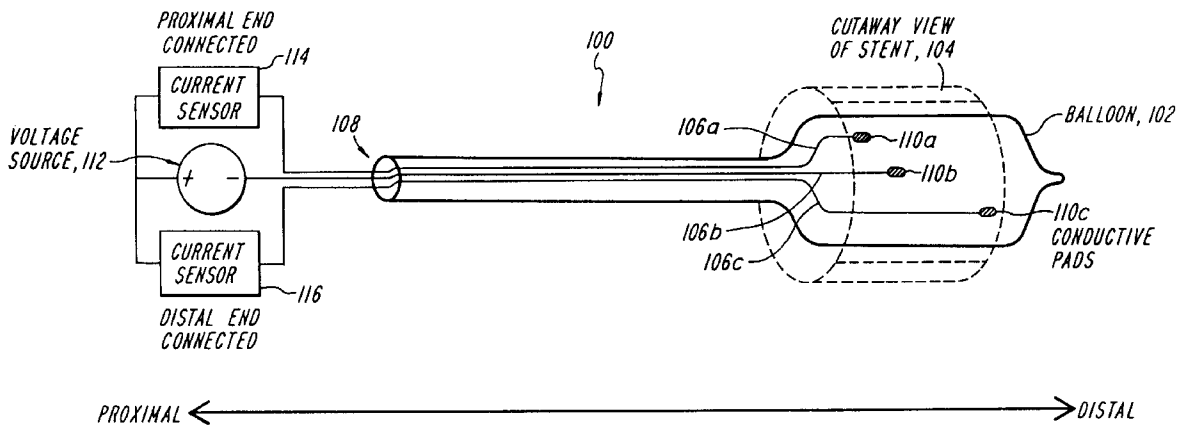
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*Primary Examiner*—Paul J. Hirsch  
*Assistant Examiner*—Michael B. Priddy  
*Attorney, Agent, or Firm*—Samuels, Gauthier & Stevens, LLP

[57] **ABSTRACT**

An endoluminal device slippage sensor system including an electrically conductive endoluminal device and a catheter assembly to which the device is coupled for deployment into a lumen. First, second and third electrodes are associated with the catheter assembly, each respectively in direct electrical contact with a proximal, a middle and a distal portion of the device. A potential source generates a potential between the first and second electrodes and between the second and third electrodes. The potential between the electrodes is varied in accordance with a change of position of the device along the axis of the catheter during deployment in which the proximal or distal portion of the device is disconnected from the first or third electrode, respectively. In accordance with another embodiment of the invention there is provided an endoluminal device slippage sensor system including an electrically conductive endoluminal device and a catheter assembly to which the device is coupled for deployment into a lumen. At least two electrodes are mounted longitudinally along the length of the catheter assembly, each of the electrodes being in direct electrical contact with the device. A potential source generates a potential between the electrodes, the potential between the electrodes being varied in accordance with a change of position of the device along the axis of the catheter assembly.

**15 Claims, 3 Drawing Sheets**



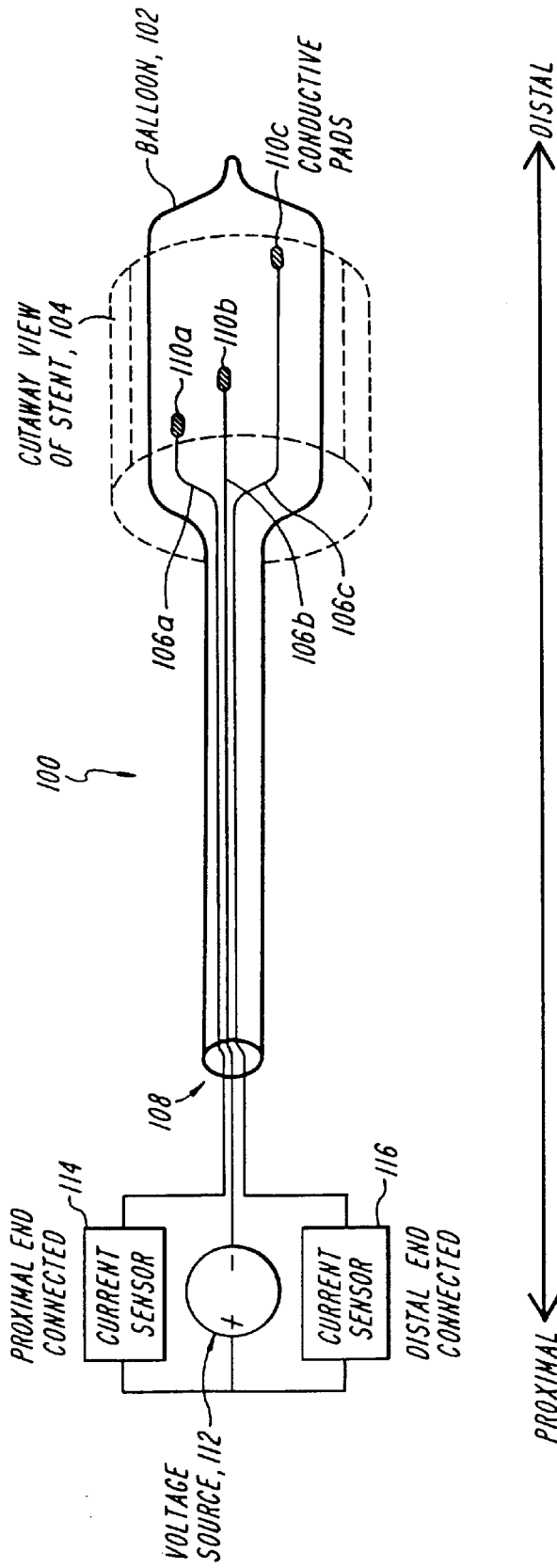


FIG. 1

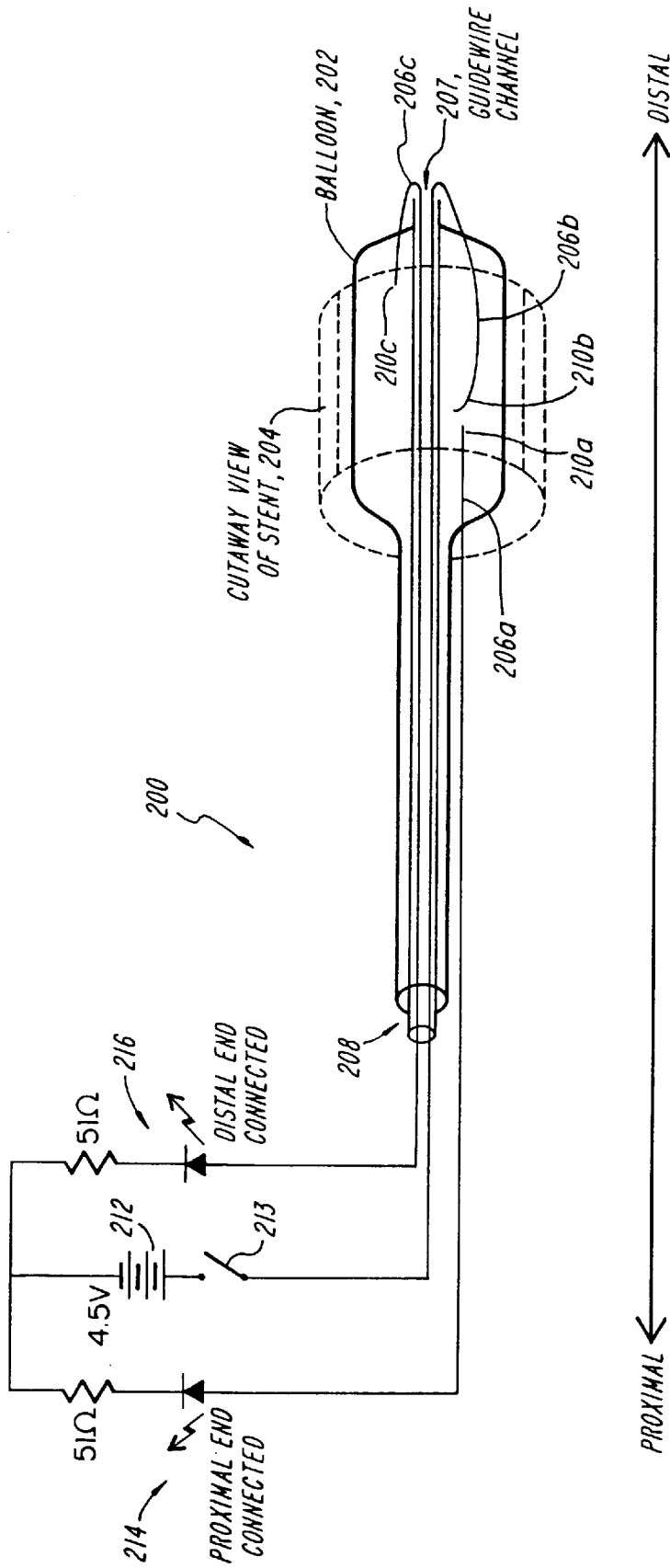


FIG. 2

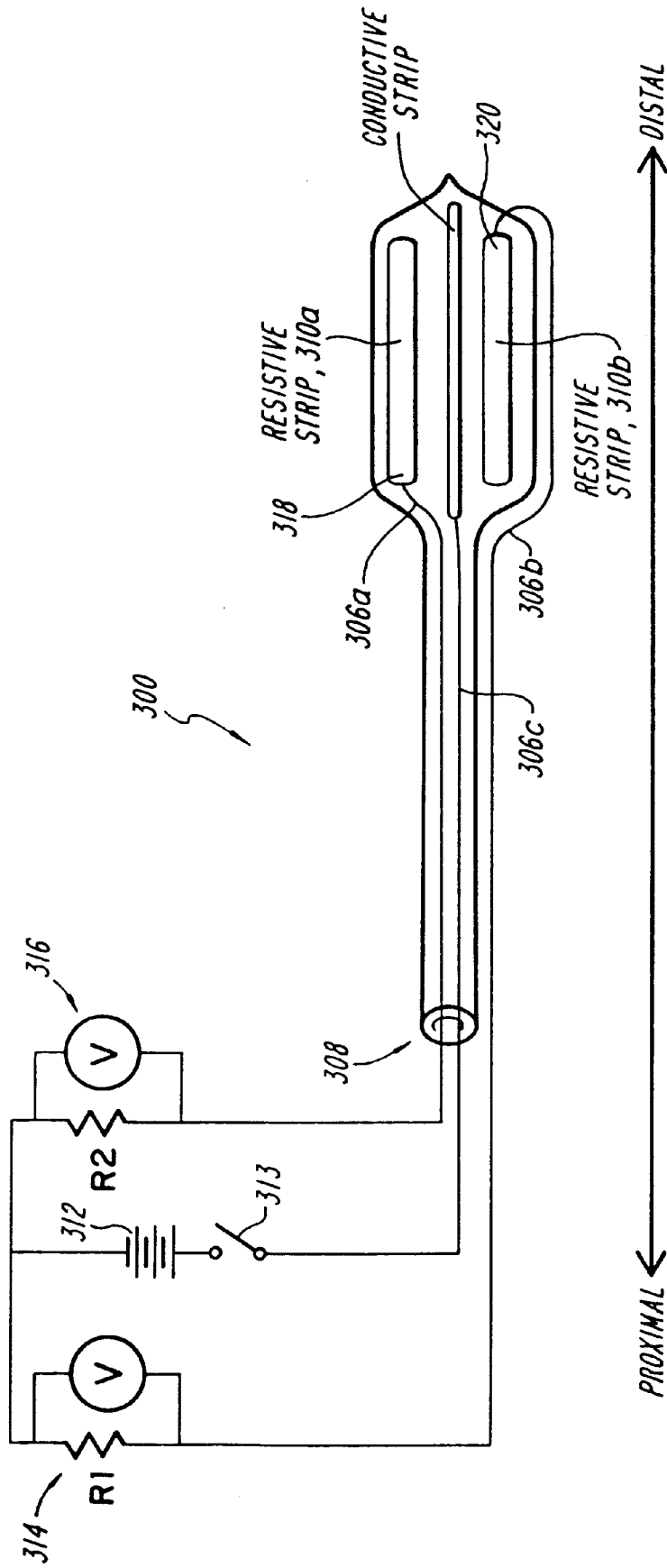


FIG. 3

## STENT SLIP SENSING SYSTEM AND METHOD

### PRIORITY INFORMATION

This application claims priority from provisional application Ser. No. 60/085,097 filed May 12, 1998.

### BACKGROUND OF THE INVENTION

The invention relates to the field of catheter delivered stents, and in particular to a catheter slip sensor.

Slippage or loosening of a stent on the delivery catheter impairs the accuracy of stent placement in up to 10% of all procedures, yet current stent delivery technologies do not inform the operator of slip until after the stent is irreversibly expanded. This is especially important given the rapidly increasing popularity of many stent designs (there were over 200,000 endovascular stents implanted in the U.S. in 1996) and the fact that clinical failure of a stent implantation may occur with placement errors as small as a few millimeters.

An endovascular stent is a hollow, expandable tubular structure that is mounted over a catheter and is threaded through a hemostatic valve into the vasculature. Once positioned, it is expanded by either inflating a lumenally-mounted balloon or by retracting a restraining sheath that permits the elastic stent to spring open.

Slippage can occur as the stent passes into the artery through the hemostatic valve, or more commonly, while navigating tortuous vasculature. This second cause of slip occurs in a two-stage process: leading edge separation and edge snare. As the catheter is pushed through a sharp curvature, it bends more abruptly than the stent. This causes a separation between the catheter and the distal end of the stent along the outer edge of the curvature. The leading edge of the stent now protrudes beyond the catheter profile, and becomes ensnared in the arterial bend.

Stent slip on the delivery catheter is difficult to directly measure. The majority of endovascular stent designs, including the two currently approved by the FDA, are only slightly radio-opaque, making stent placement difficult. The majority of stenting systems crimp the stent over radio-opaque markers on the delivery catheter to provide the operator with indirect evidence of the stent location under fluoroscopy. This indirect method is inaccurate and misleading if the stent slips. The operator, unaware of the displacement, may attempt to deploy the stent once the catheter markings are positioned within the stenosed region, resulting in inaccurate placement, incomplete expansion, or total nondeployment of the stent. The success of the stent positioning can be ascertained only after deployment, through indirect angiographic evidence of the flow patterns of radio-opaque dye through the stented vessel.

There are more serious ramifications of the operator being unaware of a displaced stent than inaccurate placement. If the stent begins to loosen on its delivery catheter it can slide off entirely once its protective sheath is retracted. If the stent dislodges in the distal direction it may enter into the circulation, requiring emergency surgery for retrieval. If it slides too far proximally it will not deploy and then can later slip over the balloon in the distal direction as the balloon is being retracted into the guide catheter. These issues could be avoided if the operator could sense displacement of the stent along the delivery catheter, as the operator could then opt to either retrieve and recrimp the stent before retracting the guide catheter or deploy the stent immediately before greater risk of stent displacement is encountered.

The danger of stent movement on the guide catheter is evinced by the variety of means that have been proposed to negate it. As discussed below, none have proved entirely effective. There is a device that detects the presence or absence of the distal region of a stent against the catheter, but it cannot measure the position of the stent along the catheter nor detect proximal slippage. The system we propose is capable of detecting both a proximal and distal dislodgment of the stent as well as measure the relative position of the stent against the catheter. In one embodiment it can further provide information about localized regions of detachment, such as occur just prior to axial slip when advancing the catheter past a tight arterial bend. We have constructed a prototype, as detailed below, and have demonstrated its feasibility.

### SUMMARY OF THE INVENTION

It is an object of the invention to improve upon the design of the catheter assembly used to deploy endoluminal stents. Specifically, the invention demonstrates how miniature resistive electrical sensors attached to the catheter may be employed to provide the operator with real-time information concerning the relative position of the stent relative to the catheter. This information can warn the operator of clinically important conditions such as unwanted slippage of the entire stent along the axis of the catheter during catheter placement, or separation of a region of the stent from the catheter during navigation of small-radius arterial bends.

In accordance with one embodiment of the invention there is provided an endoluminal device slippage sensor system including an electrically conductive endoluminal device and a catheter assembly to which the device is coupled for deployment into a lumen. First, second and third electrodes are associated with the catheter assembly, each respectively in direct electrical contact with a proximal, a middle and a distal portion of the device. A potential source generates a potential between the first and second electrodes and between the second and third electrodes. The potential between the electrodes is varied in accordance with a change of position of the device along the axis of the catheter assembly during deployment in which the proximal or distal portion of the device is disconnected from the first or third electrode, respectively.

In accordance with another embodiment of the invention there is provided an endoluminal device slippage sensor system including an electrically conductive endoluminal device and a catheter assembly to which the device is coupled for deployment into a lumen. At least two electrodes are mounted longitudinally along the length of the catheter assembly, each of the electrodes being in direct electrical contact with the device. A potential source generates a potential between the electrodes, the potential between the electrodes being varied in accordance with a change of position of the device along the axis of the catheter assembly.

### BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a functional block diagram of a stent slippage sensing system in accordance with the invention;

FIG. 2 is a functional block diagram of an alternative embodiment of a stent slippage sensing system; and

FIG. 3 is a functional block diagram of another alternative embodiment of a stent slippage sensing system.

### DETAILED DESCRIPTION OF THE INVENTION

FIG. 1 is a functional block diagram of a stent slip sensing system **100** in accordance with the invention. The system

includes a delivery balloon catheter **102** and a stent **104** that is positioned at the distal end of the catheter. The stent is shown in a cutaway view. Three conductors **106a**, **106b**, **106c** run from a proximal port **108** of the catheter (held by the operator) to the outer surface of the balloon. The conductors are surrounded by insulation except at their terminus on the balloon, where they are bared to form conductive pads **110a**, **110b**, **110c**. The conductive pads are positioned at each of the proximal, one-third or mid-proximal, and distal ends of the balloon, respectively.

The electrically conductive stent is mounted over the conductors, sandwiching them in place next to the balloon. A small voltage difference is applied from a voltage source **112** between the middle conductor **106b** and each of the end conductors **106a**, **106c**. The current that flows from the center conductive pad **110b**, through the stent **104**, and out the end conductors **110a**, **110c** is monitored via current sensors **114**, **116**. If the stent begins to slip in the distal direction away from the operator, current will cease through the proximally mounted conductive pad **110a**. Similarly, a proximal slip of the stent will stop current through the distal conductive pad **110c**. The voltage source is current-limited to  $<10 \mu\text{A}$  at a frequency of 1 kHz to comply with FDA regulations.

FIG. 2 is a functional block diagram of a stent slip sensing system **200** in accordance with an alternative embodiment of the invention. The system **200** includes a balloon catheter **202** and a stent **204**. The catheter, for example, can be a 3 mm compliant angioplasty type as manufactured by Advanced Cardiovascular Systems (ACS). The stent, for example, can be a 3 mm MultiLink stent as manufactured by ACS.

Three 40 gauge enameled copper wires run from a proximal port **208** of the catheter (held by the operator) to the outer surface of the balloon. Each of the wires has a 1 mm bared end for use as a conductive region **210a**, **210b**, **210c**. The conductive regions could alternatively be configured from a conductive polymer embedded into the catheter or a metallic foil lining the catheter stem.

Two of the wires **206b**, **206c** are threaded through a mechanical guide wire channel **207** of the catheter. The third wire **206a** is wrapped on the outside of the catheter. The proximal wire ends are secured in place by wrapping them around the catheter base, and the distal ends are secured and electrically connected by crimping them onto the balloon. Different sensitivities of slip can be obtained by varying the offset between the distal/middle and proximal/middle pairs of contacts.

A small voltage difference is applied from a voltage source **212** via a switch **213** between the middle conductor **206b** and each of the end conductors **206a**, **206c**. The current that flows from the center conductive pad **210b**, through the stent **204**, and out the end conductors **210a**, **210c** is monitored via current sensors **214**, **216**. Electrical resistance varies from approximately  $25 \Omega$  when connected, to more than  $10 \text{ k}\Omega$  when slip occurs in a ionic (PBS) bath that simulates a blood/vascular tissue environment. To comply with FDA regulations, in clinical use the contact sensor would be driven by an alternating current voltage source, typically 10 kHz, that would be current limited to  $10 \mu\text{A}$ . In a prototype system, a 6-volt battery DC source is used to generate the difference in sensor resistance so as to drive a light-emitting diode through a current limiting  $51 \Omega$  resistor.

In another alternative embodiment of the invention, a continuous measurement of the location of the stent relative to the catheter is obtained. FIG. 3 is a functional block

diagram of a stent slip sensing system **300**. The system **300** includes a balloon catheter **302** and an electrically conductive stent (not shown). A pair of resistive strips **310a**, **310b** are mounted axially along the length of the balloon catheter, and a third conductive strip **311** is mounted on the catheter parallel to, but not touching the resistive strips. The strips also include conductive wires **306a**, **306b**, **306c**, respectively, coupled to a proximal port **308**. The resistive strips **310a**, **310b** can be fabricated from a material such as Nichrome, and the conductive strip **311** from a material such as aluminum. Each strip can be, for example,  $50 \mu\text{m}$  thick, 0.5 mm wide, and 3 mm long. When the stent is positioned on the catheter, it is in electrical contact with each of the strips.

A voltage/current source **312** (e.g.  $100 \mu\text{A}$ ) supplies a current to the center conductive strip **311** via a switch **313**, which then flows through the electrically-conductive stent and into both resistive strips. The current next proceeds out the proximal end **318** of one resistive strip and the distal end **320** of the other resistive strip, through fixed resistors **R1** and **R2** of two voltage sensors **314**, **316**, and back into the voltage/current source. Resistors **R1** and **R2** each form voltage dividers with the resistive strips, and the voltage developed across them is monitored. The resistance of the fixed resistors **R1** and **R2** should be of the same magnitude as the resistance of the resistive strips, which for the Nichrome example illustrated is approximately  $500 \Omega$ .

When the stent is properly positioned it shorts both resistive strips to the conductive strip, and the entire voltage from the voltage source is developed across **R1** and **R2**. As the stent slips proximally, current must flow through a portion of the distally attached resistive strip **310b**, and the resultant decrease in voltage drop across **R1** measures the new proximal stent position. As the stent slips distally, a similar decrease in the voltage developed across **R2** tracks the distal position. A further improvement would add more resistive strips with alternating proximal and distal attachment points evenly spaced around the balloon catheter surface. This would permit detection and measurement of localized regions of stent/catheter detachment, such as occurs when passing the catheter around tight arterial bends just prior to stent slip.

Although the present invention has been shown and described with respect to several preferred embodiments thereof, various changes, omissions and additions to the form and detail thereof, may be made therein, without departing from the spirit and scope of the invention. For example, while the invention is illustrated using a cardiac endovascular stent as the most commonly used variety of stent, it will be appreciated that the system of the invention could be successfully used to deploy and measure slippage of any expandable endoluminal device.

What is claimed is:

1. An endoluminal device slippage sensor system comprising:
  - an electrically conductive endoluminal device;
  - a catheter assembly to which said device is coupled for deployment into a lumen;
  - first, second and third electrodes associated with said catheter assembly, each respectively in direct electrical contact with a proximal, a middle and a distal portion of said device; and
  - a potential source which generates a potential between said first and second electrodes and between said second and third electrodes, said potential between said electrodes being varied in accordance with a change of

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position of said device along the axis of said catheter assembly during deployment in which said proximal or distal portion of said device is disconnected from said first or third electrode, respectively.

2. The system of claim 1, wherein said endoluminal device comprises an endovascular stent. 5

3. The system of claim 1, wherein said catheter assembly comprises a balloon catheter.

4. The system of claim 1 further comprising at least one potential sensor which monitors the potential variations between said electrodes. 10

5. The system of claim 1, wherein said potential source comprises a voltage source.

6. An endoluminal device slippage sensor system comprising: 15

- an electrically conductive endoluminal device;
- a catheter assembly to which said device is coupled for deployment into a lumen;

at least two electrodes mounted longitudinally along the length of said catheter assembly, each of said electrodes being in direct electrical contact with said device; and 20  
a potential source which generates a potential between said electrodes, said potential between said electrodes being varied in accordance with a change of position of said device along the axis of said catheter assembly. 25

7. The system of claim 6, wherein said endoluminal device comprises an endovascular stent.

8. The system of claim 1, wherein said catheter assembly comprises a balloon catheter. 30

9. The system of claim 1 further comprising at least one potential sensor which monitors the potential variations between said electrodes.

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10. The system of claim 1, wherein said potential source comprises a voltage source.

11. The system of claim 1 further comprising at least a third electrode mounted longitudinally along the length of said catheter assembly and being in direct electrical contact with said device.

12. The system of claim 11, wherein said at least two electrodes comprise resistive electrodes.

13. The system of claim 12, wherein said at least a third electrode comprises a conductive electrode.

14. A method of sensing slippage of an electrically conductive endoluminal device which is coupled to a catheter assembly for deployment into a lumen, comprising:

- providing at least two electrodes longitudinally along the length of said catheter assembly, each of said electrodes being in direct electrical contact with said device; and
- generating a potential between said electrodes, said potential between said electrodes being varied in accordance with a change of position of said device along the axis of said catheter assembly.

15. A method of sensing slippage of an electrically conductive endoluminal device which is coupled to a catheter assembly for deployment into a lumen, comprising:

- providing at least two electrodes longitudinally along the length of said catheter assembly, each of said electrodes being in direct electrical contact with said device; and
- generating a potential between said electrodes, said potential between said electrodes being varied in accordance with a change of position of said device along the axis of said catheter assembly.

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